HI5721

## Features

- Throughput Rate . . . . . . . . . . . . . . . . . . . . . 125 MSPS
- Low Power . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 700 mW
- Integral Linearity Error . . . . . . . . . . . . . . . . . . . . 1.5 LSB
- Low Glitch Energy
.1.5pV•s
- TTL/CMOS Compatible Inputs
- Improved Hold Time $\qquad$ 0.5ns
- Excellent Spurious Free Dynamic Range
- Improved Second Source for the AD9721


## Applications

- Wireless Communications
- Direct Digital Frequency Synthesis
- Signal Reconstruction
- HDTV
- Test Equipment
- High Resolution Imaging Systems
- Arbitrary Waveform Generators


## Description

The HI5721 is a 10-bit, 125 MSPS, high speed D/A converter. The converter incorporates a 10-bit, input data register with quadrature data logic capability and current outputs. The HI5721 features low glitch energy and excellent frequency domain specifications.

## Ordering Information

| PART <br> NUMBER | TEMP. <br> RANGE $\left({ }^{\circ} \mathbf{C}\right)$ | PACKAGE | PKG. <br> NO. |
| :--- | :---: | :--- | :---: |
| HI5721BIP | -40 to 85 | 28 Ld PDIP | E28.6 |
| HI5721BIB | -40 to 85 | 28 Ld SOIC (W) | M28.3 |
| HI5721-EVP | 25 | Evaluation Board (PDIP) |  |
| HI5721-EVS | 25 | Evaluation Board (SOIC) |  |

## Pinout

|  | $\begin{gathered} \text { HI5721 } \\ \text { (PDIP, SOIC) } \\ \text { TOP VIEW } \end{gathered}$ |  |
| :---: | :---: | :---: |
| D9 (MSB) 1 | $\checkmark$ | 28 DGND |
| D8 2 |  | 27 DV EE |
| D7 3 |  | 26 CTRL AMP IN |
| D6 4 |  | 25 REF OUT |
| D5 5 |  | 24 CTRL AMP OUT |
| D4 6 |  | 23 REF IN |
| D3 7 |  | 22 AV EE |
| D2 8 |  | 21 Iout |
| D1 9 |  | 20 Iout |
| D0 (LSB) 10 |  | 19 ARTN |
| CLOCK 11 |  | 18 AGND |
| NC 12 |  | $17 \mathrm{R}_{\text {SET }}$ |
| INVERT 13 |  | 16 DV EE |
| $\mathrm{V}_{\mathrm{Cc}} 14$ |  | 15 DGND |

## Typical Applications Circuit



Functional Block Diagram



## Thermal Information


Maximum Junction Temperature
HI5721BIx
$.150^{\circ} \mathrm{C}$
Maximum Storage Temperature Range . . . . . . . . . $-65^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$
Maximum Lead Temperature (Soldering 10s) . . . . . . . . . . . . . $300^{\circ} \mathrm{C}$
(SOIC - Lead Tips Only)

## Operating Conditions

Temperature Range $\qquad$ $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$

CAUTION: Stresses above those listed in "Absolute Maximum Ratings" may cause permanent damage to the device. This is a stress only rating and operation of the device at these or any other conditions above those indicated in the operational sections of this specification is not implied.

NOTE:

1. $\theta_{\mathrm{JA}}$ is measured with the component mounted on an evaluation PC board in free air.

Electrical Specifications $\quad A V_{E E}, D V_{E E}=-4.94$ to $-5.46 \mathrm{~V}, \mathrm{~V}_{\mathrm{CC}}=+4.75$ to $+5.25 \mathrm{~V}, \mathrm{CTRL} A M P I N=R E F ~ O U T$, $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ for All Typical Values

| PARAMETER | TEST CONDITIONS | $\begin{gathered} \mathrm{H} 15721 \mathrm{BI} \\ \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C} \text { TO } 85^{\circ} \mathrm{C} \end{gathered}$ |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX |  |
| SYSTEM PERFORMANCE |  |  |  |  |  |
| Resolution |  | 10 | - | - | Bits |
| Integral Linearity Error, INL | (Note 4) ("Best Fit" Straight Line) | - | $\pm 0.5$ | $\pm 1.5$ | LSB |
| Differential Linearity Error, DNL | (Note 4) | - | $\pm 0.5$ | $\pm 1.0$ | LSB |
| Offset Error, IOS | (Note 4) | - | 16 | 75 | $\mu \mathrm{A}$ |
| Full Scale Gain Error, FSE | (Notes 2, 4) | - | 2 | 10 | \% |
| Offset Drift Coefficient | (Note 3) | - | 0.1 | - | $\mu \mathrm{A} /{ }^{\circ} \mathrm{C}$ |
| Full Scale Output Current, $\mathrm{I}_{\text {FS }}$ |  | - | -20.48 | - | mA |
| Output Voltage Compliance Range | (Note 3) | -1.5 | - | +3.0 | V |

DYNAMIC CHARACTERISTICS

| Throughput Rate | (Note 3) | 125.0 | - | - | MSPS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Output Voltage Full Scale Step Settling Time, tsETT FS | To $\pm 0.5$ LSB Error Band $\mathrm{R}_{\mathrm{L}}=50 \Omega$ (Note 3) | - | 4.5 | - | ns |
| Output Voltage Small Step Settling Time, SETT SM | 100 mV Step to $\pm 0.5$ LSB Error Band, $\mathrm{R}_{\mathrm{L}}=50 \Omega$ (Note 3) | - | 3.5 | - | ns |
| Singlet Glitch Area, GE (Peak Glitch) | $\mathrm{R}_{\mathrm{L}}=50 \Omega$ (Note 3) | - | 3.5 | - | pV•s |
| Doublet Glitch Area, (Net Glitch) |  | - | 1.5 | - | pV •s |
| Output Slew Rate | $R_{L}=50 \Omega$, DAC Operating in Latched Mode (Note 3) | - | 1,000 | - | V/us |
| Output Rise Time | $R_{L}=50 \Omega$, DAC Operating in Latched Mode (Note 3) | - | 675 | - | ps |
| Output Fall Time | $R_{L}=50 \Omega$, DAC Operating in Latched Mode (Note 3) | - | 470 | - | ps |

Electrical Specifications $\quad A V_{E E}, D V_{E E}=-4.94$ to $-5.46 \mathrm{~V}, \mathrm{~V}_{\mathrm{CC}}=+4.75$ to $+5.25 \mathrm{~V}, \mathrm{CTRL} A M P \mathrm{IN}=$ REF OUT, $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ for All Typical Values (Continued)

| PARAMETER | TEST CONDITIONS | $\begin{gathered} \mathrm{H} / 5721 \mathrm{BI} \\ \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C} \text { TO } 85^{\circ} \mathrm{C} \end{gathered}$ |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX |  |
| Spurious Free Dynamic Range, SFDR to Nyquist | $\begin{aligned} & \mathrm{f}_{\mathrm{CLK}}=125 \mathrm{MSPS}, \text { fout }=2.02 \mathrm{MHz}, 62.5 \mathrm{MHz} \\ & \text { Span (Notes 3, 5) } \end{aligned}$ | - | -59 | - | dBc |
|  | $\begin{aligned} & \mathrm{f}_{\mathrm{f} \text { LK }}=125 \mathrm{MSPS}, \mathrm{f} \text { OUT }=25 \mathrm{MHz}, 62.5 \mathrm{MHz} \\ & \text { Span (Notes 3, 5) } \end{aligned}$ | - | -53 | - | dBc |
|  | $\begin{aligned} & \mathrm{f}_{\mathrm{f} \text { LK }}=100 \mathrm{MSPS}, \mathrm{fOUT}=2.02 \mathrm{MHz}, 50 \mathrm{MHz} \\ & \text { Span (Notes 3, 5) } \end{aligned}$ | - | -59 | - | dBc |
|  | ${ }^{\mathrm{f}} \mathrm{CLK}=100 \mathrm{MSPS}, \mathrm{f}_{\mathrm{OUT}}=25 \mathrm{MHz}, 50 \mathrm{MHz}$ Span (Notes 3, 5) | - | -51 | - | dBc |
| Spurious Free Dynamic Range, SFDR Within a Window | ${ }^{\mathrm{f}} \mathrm{CLK}=125 \mathrm{MSPS}, \mathrm{f}_{\mathrm{OUT}}=2.02 \mathrm{MHz}, 2 \mathrm{MHz}$ Span (Notes 3, 5) | - | -75 | - | dBc |
|  | $\mathrm{f}_{\mathrm{CLK}}=125 \mathrm{MSPS}, \mathrm{f}_{\mathrm{OUT}}=25 \mathrm{MHz}, 2 \mathrm{MHz}$ Span (Notes 3, 5) | - | -70 | - | dBc |
|  | $\mathrm{f}_{\mathrm{CLK}}=100 \mathrm{MSPS}, \mathrm{f}_{\mathrm{OUT}}=2.02 \mathrm{MHz}, 2 \mathrm{MHz}$ Span (Notes 3, 5) | - | -75 | - | dBc |
|  | $\mathrm{f}_{\mathrm{CLK}}=100 \mathrm{MSPS}, \mathrm{fOUT}=25 \mathrm{MHz}, 2 \mathrm{MHz}$ Span (Notes 3, 5) | - | -72 | - | dBc |
| Signal to Noise Ratio (SNR) to Nyquist (Ignoring the First 5 Harmonics) | $\begin{aligned} & f_{\text {CLK }}=125 \mathrm{MSPS}, \text { fout }=2.02 \mathrm{MHz} \text {, } \\ & (\text { Notes } 3,5) \end{aligned}$ | - | 54 | - | dB |
|  | $\begin{aligned} & \mathrm{f}_{\mathrm{CLK}}=125 \mathrm{MSPS}, \mathrm{f} \text { OUT }=25 \mathrm{MHz} \\ & (\text { Notes 3, } 5) \end{aligned}$ | - | 51.5 | - | dB |
|  | $\begin{aligned} & \mathrm{f} \mathrm{CLK}=100 \mathrm{MSPS}, \mathrm{fOUT}=2.02 \mathrm{MHz}, \\ & (\text { Notes 3, } 5 \text { ) } \end{aligned}$ | - | 54.5 | - | dB |
|  | $\begin{aligned} & \mathrm{f}_{\mathrm{CLK}}=100 \mathrm{MSPS}, \mathrm{f} \text { OUT }=25 \mathrm{MHz} \\ & (\text { Notes 3, 5) } \end{aligned}$ | - | 50.3 | - | dB |
| Signal to Noise Ratio + Distortion (SINAD) to Nyquist | $\begin{aligned} & \text { fCLK }=125 \text { MSPS, fout }=2.02 \mathrm{MHz}, \\ & (\text { Notes 3, } 5 \text { ) } \end{aligned}$ | - | 52.4 | - | dB |
|  | $\begin{aligned} & \text { fCLK }=125 \text { MSPS, fout }=25 \mathrm{MHz} \\ & (\text { Notes } 3,5) \end{aligned}$ | - | 49.2 | - | dB |
|  | $\begin{aligned} & \mathrm{f}_{\mathrm{CLK}}=100 \mathrm{MSPS}, \mathrm{fOUT}=2.02 \mathrm{MHz}, \\ & (\text { Notes 3, } 5) \end{aligned}$ | - | 52.7 | - | dB |
|  | $\begin{aligned} & \mathrm{f} \mathrm{fLK}=100 \mathrm{MSPS}, \mathrm{fOUT}=25 \mathrm{MHz} \\ & (\text { Notes 3, } 5) \end{aligned}$ | - | 47.6 | - | dB |
| Total Harmonic Distortion (THD) to Nyquist | $\begin{aligned} & \mathrm{f} \mathrm{CLK}=125 \mathrm{MSPS}, \mathrm{f} \text { OUT }=2.02 \mathrm{MHz} \text {, } \\ & (\text { Notes 3, } 5 \text { ) } \end{aligned}$ | - | -57.8 | - | dBc |
|  | $\begin{aligned} & \mathrm{f}_{\mathrm{CLK}}=125 \mathrm{MSPS}, \mathrm{f} \text { OUT }=25 \mathrm{MHz} \\ & (\text { Notes } 3,5) \end{aligned}$ | - | -53.3 | - | dBc |
|  | $\begin{aligned} & \text { fCLK }=100 \mathrm{MSPS}, \text { fout }=2.02 \mathrm{MHz}, \\ & (\text { Notes 3, } 5 \text { ) } \end{aligned}$ | - | -57.9 | - | dBc |
|  | $\begin{aligned} & \mathrm{f}_{\mathrm{CLK}}=100 \mathrm{MSPS}, \mathrm{fOUT}=25 \mathrm{MHz} \\ & (\text { Notes } 3,5) \end{aligned}$ | - | -51 | - | dBc |
| Intermodulation Distortion (IMD) to Nyquist | $\begin{aligned} & \mathrm{f}_{\mathrm{CLK}}=125 \mathrm{MSPS}, \mathrm{f} \text { OUT1 }=800 \mathrm{kHz}, \\ & \mathrm{f} \text { OUT2 }=900 \mathrm{kHz}(\text { Notes } 3,5) \end{aligned}$ | - | 57.3 | - | dB |
|  | $\begin{aligned} & \mathrm{f}_{\mathrm{CLK}}=100 \mathrm{MSPS}, \mathrm{f}_{\mathrm{OUT} 1}=800 \mathrm{kHz}, \\ & \mathrm{f}_{\mathrm{OUT} 2}=900 \mathrm{kHz}(\text { Notes } 3,5) \end{aligned}$ | - | 57.2 | - | dB |

Electrical Specifications $\quad A V_{E E}, D V_{E E}=-4.94$ to $-5.46 \mathrm{~V}, \mathrm{~V}_{\mathrm{CC}}=+4.75$ to $+5.25 \mathrm{~V}, \mathrm{CTRL} A M P \mathrm{IN}=$ REF OUT, $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ for All Typical Values (Continued)

| PARAMETER | TEST CONDITIONS | $\begin{gathered} \mathrm{HI} 5721 \mathrm{BI} \\ \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C} \text { TO } 85^{\circ} \mathrm{C} \end{gathered}$ |  |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX |  |
| REFERENCE/CONTROL AMPLIFIER |  |  |  |  |  |
| Internal Reference Voltage, REF OUT | (Note 4) | -1.15 | -1.25 | -1.35 | V |
| Internal Reference Voltage Drift | (Note 3) | - | 100 | - | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Internal Reference Output Current Sink/Source Capability | (Note 3) | -50 | - | +500 | $\mu \mathrm{A}$ |
| Amplifier Input Impedance | (Note 3) | - | 10 | - | $\mathrm{M} \Omega$ |
| Amplifier Large Signal Bandwidth | 4.0V $\mathrm{V}_{\text {P-P }}$ Sine Wave Input, to Slew Rate Limited (Note 3) | - | 1 | - | MHz |
| Amplifier Small Signal Bandwidth | $1.0 \mathrm{~V}_{\text {P-P }}$ Sine Wave Input, to -3dB Loss (Note 3) | - | 10 | - | MHz |
| Reference Input Impedance | (Note 3) | - | 4.6 | - | $\mathrm{k} \Omega$ |
| Reference Input Multiplying Bandwidth | $R_{L}=50 \Omega, 100 \mathrm{mV}$ Sine Wave, to -3 dB Loss at IOUT (Note 3) | - | 75 | - | MHz |
| DIGITAL INPUTS (D9-D0, CLK, INVERT) |  |  |  |  |  |
| Input Logic High Voltage, $\mathrm{V}_{\mathrm{IH}}$ | (Note 4) | 2.0 | - | - | V |
| Input Logic Low Voltage, $\mathrm{V}_{\text {IL }}$ | (Note 4) | - | - | 0.8 | V |
| Input Logic Current, $\mathrm{I}_{\mathrm{IH}}$ | (Note 4) | - | - | 400 | $\mu \mathrm{A}$ |
| Input Logic Current, IIL | (Note 4) | - | - | 700 | $\mu \mathrm{A}$ |
| Digital Input Capacitance, $\mathrm{C}_{\text {IN }}$ | (Note 3) | - | 3.0 | - | pF |
| TIMING CHARACTERISTICS |  |  |  |  |  |
| Data Setup Time, tsu | See Figure 3 (Note 3) | 2.0 | - | - | ns |
| Data Hold Time, thLD | See Figure 3 (Note 3) | 0.5 | - | - | ns |
| Propagation Delay Time, tpd | See Figure 3 (Note 3) | - | 4.5 | - | ns |
| CLK Pulse Width, tpW1, tPW2 | See Figure 3 (Note 3) | 1.0 | 0.85 | - | ns |
| POWER SUPPLY CHARACTERISITICS |  |  |  |  |  |
| $\mathrm{IAV}_{\text {EE }}$ | (Note 4) | - | 100 | 110 | mA |
| IDV ${ }_{\text {EE }}$ | (Note 4) | - | - | 15 | mA |
| $\mathrm{V}_{\mathrm{CC}}$ | (Note 4) | - | 14 | 25 | mA |
| Power Dissipation | (Note 4) | - | 700 | 775 | mW |
| Power Supply Rejection Ratio | $\mathrm{V}_{\mathrm{CC}} \pm 5 \%, \mathrm{~V}_{\mathrm{EE}} \pm 5 \%$ | - | 50 | - | $\mu \mathrm{A} / \mathrm{V}$ |

NOTES:
2. Gain Error measured as the error in the ratio between the full scale output current and the current through R $\mathrm{RET}_{\text {SE }}$ (typically $640 \mu \mathrm{~A}$ ). Ideally the ratio should be 32.
3. Parameter guaranteed by design or characterization and not production tested.
4. All devices are $100 \%$ tested at $25^{\circ} \mathrm{C}$. $100 \%$ productions tested at temperature extremes for military temperature devices, sample tested for industrial temperature devices.
5. Spectral measurements made without external filtering.

## Timing Diagrams



FIGURE 1. FULL SCALE SETTLING TIME DIAGRAM


FIGURE 2. PEAK GLITCH AREA (SINGLET) MEASUREMENT METHOD


FIGURE 3. PROPAGATION DELAY, SETUP TIME, HOLD TIME AND MINIMUM PULSE WIDTH DIAGRAM

## Typical Performance Curves



FIGURE 4. INTEGRAL NON-LINERARITY "BEST FIT" STRAIGHT LINE


FIGURE 6. SPURIOUS FREE DYNAMIC RANGE TO NYQUIST 25MHz FUNDAMENTAL


FIGURE 8. INTERMODULATION DISTORTION


FIGURE 5. DIFFERENTIAL NON-LINEARITY


FIGURE 7. SPURIOUS FREE DYNAMIC RANGE TO NYQUIST 2MHz FUNDAMENTAL


FIGURE 9. SPURIOUS FREE DYNAMIC RANGE (TO NYQUIST) vs OUTPUT FREQUENCY

Typical Performance Curves (Continued)


FIGURE 10. SPURIOUS FREE DYNAMIC RANGE ( $\pm 1 \mathrm{MHz}$ WINDOW) vs FREQUENCY


FIGURE 12. SIGNAL TO NOISE + DISTORTION vs OUTPUT FREQUENCY


FIGURE 14. GAIN ERROR vs TEMPERATURE


FIGURE 11. SIGNAL TO NOISE RATIO vs OUTPUT FREQUENCY


FIGURE 13. TOTAL HARMONIC DISTORTION vs OUTPUT FREQUENCY


FIGURE 15. OFFSET ERROR vs TEMPERATURE

## Typical Performance Curves (Continued)



FIGURE 16. REFERENCE VOLTAGE vs TEMPERATURE


NOTE: Clock Frequency does not alter power dissipation. FIGURE 17. POWER DISSIPATION vs TEMPERATURE

## Pin Descriptions

| PIN NO. | PIN NAME | PIN DESCRIPTION |
| :---: | :---: | :---: |
| 1-10 | D0 (LSB) through D9 (MSB) | Digital Data Bit 0, the Least Significant Bit through Digital Data Bit 9, the Most Significant Bit. |
| 11 | CLK | Data Clock pin 100kHz to 125 MSPS. |
| 12 | NC | No Connect. |
| 13 | INVERT | Data Invert control for bits D0 (LSB) through D8. D9 (MSB) is not affected. |
| 14 | $\mathrm{V}_{\mathrm{CC}}$ | Digital Logic Supply +5V. |
| 15, 28 | DGND | Digital Ground. |
| 16, 27 | DVEE | -5.2V Logic Supply. |
| 17 | $\mathrm{R}_{\text {SET }}$ | External resistor to set the full scale output current. $\mathrm{I}_{\text {FS }}=32 \times$ (CTRL AMP IN/RSET). Typically $1960 \Omega$. |
| 18 | AGND | Analog Ground supply current return pin. |
| 19 | ARTN | Analog Signal Return for the R/2R ladder. |
| 20 | Iout | Current Output pin. |
| 21 | lout | Complementary Current Output pin. |
| 22 | $\mathrm{AV}_{\mathrm{EE}}$ | -5.2V Analog Supply. |
| 23 | REF IN | Reference Input pin. Typically connected to CTRL AMP OUT and a $0.1 \mu \mathrm{~F}$ capacitor should be connected to $A V_{E E}$ to bypass the reference voltage. Provides a reference for the current switching network. |
| 24 | CTRL AMP OUT | Control Amplifier Output. Used to convert the internal reference or an external signal to the precision reference current. |
| 25 | REF OUT | Internal Reference Output. Output of the internal -1.25V (typical) bandgap voltage reference. |
| 26 | CTRL AMP IN | Control Amplifier Input. High impedance, inverting input of the reference control/buffer amplifier. |

## Detailed Description

The HI5721 is a 10-bit, current out D/A converter. The DAC can convert at 125 MSPS and runs on +5 V and -5.2 V supplies. The architecture is an $R / 2 R$ and segmented switching current cell arrangement to reduce glitch and maintain 10-bit linearity without laser trimming. The HI5721 achieves its low power and high speed performance from an advanced BiCMOS process. The H15721 consumes 700 mW (typical) and has an improved hold time of only 0.5 ns (typical). The HI5721 is an excellent converter to be used for communications applications and high performance video systems.

## Digital Inputs

The HI5721 is a TTL/CMOS compatible D/A. The inputs can be inverted using the INVERT pin. When INVERT is LOW ('0') the input quadrature logic simply passes the data through unchanged.
When INVERT is HIGH (' 1 ') bits D0 (LSB) through D8 are inverted. D9 is not inverted and can be considered a sign bit when enabling this quadrature compatible mode. The INVERT function can simplify the requirements for large sine wave lookup tables in a Numerically Controlled Oscillator. The NCO used in a DDS application would only have to store or generate 90 degrees of information and then use the INVERT control to control the sign of the output waveform.

## Data Buffer/Level Shifters

Data inputs D0 (LSB) through D9 (MSB) are internally translated from TTL to ECL. The internal latch and switching current source controls are implemented in ECL technology to maintain high switching speeds and low noise characteristics.

## Decoder/Driver

The architecture employs a split $\mathrm{R} / 2 \mathrm{R}$ and Segmented Current source arrangement. Bits D0 (LSB) through D5 directly drive a typical $R / 2 R$ network to create the binary weighted current sources. Bits D6 through D9 (MSB) pass through a "thermometer" encoder that converters the incoming data into 15 individual segmented current source enables. The split architecture helps to improve glitch while maintaining 10 -bit linearity without laser trimming. The worst case glitch is more constant across the entire output transfer function.

## Clocks and Termination

The internal 10-bit register is updated on the rising edge of the clock. Since the HI5721 clock rate can run to 125 MSPS, to minimize reflections and clock noise into the part proper termination should be used. In PCB layout clock runs should be kept short and have a minimum of loads. To guarantee consistent results from board to board, controlled impedance PCBs should be used with a characteristic line impedance $Z_{O}$ of $50 \Omega$.
To terminate the clock line a shunt terminator to ground is the most effective type at a 125 MSPS clock rate. A typical value for termination can be determined by the equation:
$\mathrm{R}_{\mathrm{T}}=\mathrm{Z}_{\mathrm{O}}$,
for the termination resistor. For a controlled impedance board with a $Z_{O}$ of $50 \Omega$, the $R_{T}=50 \Omega$. Shunt termination is best used at the receiving end of the transmission line or as close to the HI5721 CLK pin as possible.


FIGURE 18. AC TERMINATION OF THE HI5721 CLOCK LINE
Rise and Fall times and propagation delay of the line will be affected by the Shunt Terminator. The terminator can be connected to DGND.

## Noise Reduction

To reduce power supply noise, separate analog and digital power supplies should be used with $0.1 \mu \mathrm{~F}$ and $0.01 \mu \mathrm{~F}$ ceramic capacitors placed as close to the body of the HI5721 as possible on the analog ( $\mathrm{A} \mathrm{V}_{\mathrm{EE}}$ ) and digital ( DV VEE ) supplies. The analog and digital ground returns should be connected together back at the device to ensure proper operation on power up. The $\mathrm{V}_{\mathrm{CC}}$ power pin should be decoupled with a $0.1 \mu \mathrm{~F}$ capacitor.

## Reference

The internal reference in the H 5721 is a -1.25 V (typical) bandgap voltage reference with a $100 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ temperature drift (typical). The internal reference should be buffered by the Control Amplifier to provide adequate drive for the segmented current cells and the R/2R resistor ladder. Reference Out (REF OUT) should be connected to the Control Amplifier Input (CTRL AMP IN). The Control Amplifier Output (CTRL AMP OUT) should be used to drive the Reference Input (REF IN) and a $0.1 \mu \mathrm{~F}$ capacitor to analog V - ( $\mathrm{AV}_{\mathrm{EE}}$ ). This improves settling time by decoupling switching noise from the analog output of the HI5721.
The Full Scale Output Current is controlled by the CTRL AMP IN pin and the set resistor ( $\mathrm{R}_{\text {SET }}$ ). The ratio is:
IOUT $($ Full Scale $)=\left(\mathrm{V}_{\text {CTRL AMP }} \mathrm{IN} / \mathrm{R}_{\text {SET }}\right) \times 32$.

## Multiplying Capability

The HI5721 can operate in two different multiplying configurations. First, using the CTRL AMP IN input pin, a -0.6 V to -1.2 V signal can be applied with a bandwidth up to 1 MHz . To increase the multiplying bandwidth, the $0.1 \mu \mathrm{~F}$ capacitor connected from REF IN to $\mathrm{AV}_{\text {EE }}$ can be reduced.


FIGURE 19. LOW FREQUENCY MULTIPLYING CIRCUIT

If higher multiplying frequencies are desired, the reference input can be directly driven. The analog signal range is -3.3 V to -4.25 V . The multiplying signal must be capacitively coupled into REF IN onto a DC bias between -3.3 V to -4.25 V (-3.8V typically).


FIGURE 20. WIDEBAND MULTIPLYING CIRCUIT

## Outputs

The outputs lout and louT are complementary current outputs. Current is steered to either lout or lout in proportion to the digital input code. The sum of the two currents is always equal to the full scale current minus one LSB. The current output can be converted to a voltage by using a load resistor. Both current outputs should have the same load resistor ( $64 \Omega$ typically). By using a $64 \Omega$ load on the output, a $50 \Omega$ effective output resistance (ROUT) is achieved due to the $227 \Omega$ ( $\pm 15 \%$ ) parallel resistance seen looking back into the output. This is the nominal value of the R2R ladder of the DAC. The $50 \Omega$ output is needed for matching the output with a $50 \Omega$ line. The load resistor should be chosen so that the effective output resistance ( $R_{\mathrm{OUT}}$ ) matches the line resistance. The output voltage is:
$\mathrm{V}_{\text {OUT }}=$ I OUT $\times$ R OUT .
lout is defined in the reference section. The compliance range of the output is from -1.5 V to 3 V , with a $1 \mathrm{~V}_{\mathrm{P}-\mathrm{P}}$ voltage swing allowed within this range. However, if it is desired that the output be offset above zero volts, it is necessary that pin 19 (ARTN) be connected to the same voltage as the load resistor, not to exceed 3 V .

## Glitch

TABLE 1. INPUT CODING vs CURRENT OUTPUT

| INPUT CODE (D9-DO) | I OUT $^{\text {(mA) }}$ | $\mathbf{I}_{\text {OUT }}$ (mA) |
| :--- | :---: | :---: |
| 1111111111 | -20.48 | 0 |
| 1000000000 | -10.24 | -10.24 |
| 0000000000 | 0 | -20.48 |

The output glitch of the HI5721 is measured by summing the area under the switching transients after an update of the DAC. Glitch is caused by the time skew between bits of the incoming digital data. Typically the switching time of digital inputs are asymmetrical meaning that the turn off time is faster than the turn on time (TTL designs). Unequal delay paths through the device can also cause one current source to change before another. To minimize this the Harris HI5721 employes an internal register, just prior to the current sources, that is updated on the clock edge. Lastly the worst case glitch usually happens at the major transition i.e., 0111111111 to 1000000000 . But in the HI5721 the glitch
is moved to the 0000011111 to 1111100000 transition. This is achieved by the split R/2R segmented current source architecture. This decreases the amount of current switching at any one time and makes the glitch practically constant over the entire output range. By making the glitch a constant size over the entire output range this effectively integrates this error out of the end application.
In measuring the output glitch of the HI5721 the output is terminated into a $64 \Omega$ load. The glitch is measured at the major carrys throughout the DAC's output range.
The glitch energy is calculated by measuring the area under the voltage-time curve. Figure 21 shows the area considered as glitch when changing the DAC output. Units are typically specified in picoVolt • seconds ( $\mathrm{pV} \cdot \mathrm{s}$ ).


FIGURE 21. GLITCH TEST CIRCUIT


FIGURE 22. GLITCH ENERGY

## Applications

## Voltage Conversion of the Output

To convert the output current of the D/A converter to a voltage, an amplifier should be used as shown in Figure 23 below. The DAC needs a $50 \Omega$ termination resistor on the lout pin to ensure proper settling. The HFA1110 has an internal feedback resistor to compensate for high frequency operation.


FIGURE 23. HIGH SPEED CURRENT TO VOLTAGE CONVERSION

## Bipolar Applications

To convert the output to a bipolar $\pm 2.0 \mathrm{~V}$ output swing the following applications circuit is recommended. The Reference can only provide $100 \mu \mathrm{~A}$ of drive, so it must be buffered to create the bipolar offset current needed to generate -2.0 V output with all bits 'off'. The output current must be converted to a voltage and then gained up and offset to produce the proper swing. Care must be taken to compensate for the output voltage swing and error.


FIGURE 24. BIPOLAR OUTPUT CONFIGURATION

## Interfacing to the HSP45106 NCO-16

The HSP45106 is a 16-bit output, Numerically-Controlled Oscillator (NCO). The HSP45106 can be used to generate various modulation schemes for Direct Digital Synthesis (DDS) applications. Figure 25 shows how to interface an HI5721 to the HSP45106.

## Interfacing to the HSP45102 NCO-12

The HSP45102 is a 12-bit output Numerically Controlled Oscillator (NCO). The HSP45102 can be used to generate various modulation schemes for Direct Digital Synthesis (DDS) applications. Figure 26 shows how to interface an HI5721 to the HSP45102.
This high level block diagram is that of a basic PSK modulator. In this example the encoder generates the PSK waveform by driving the Phase Modulation Inputs (P1, P0) of the HSP45102. The P1-0 inputs impart a phase shift to the carrier wave as defined in Table 2.

TABLE 2. PHASE MODULATION INPUT CODING

| P1 | P0 | PHASE SHIFT <br> (DEGREES) |
| :---: | :---: | :---: |
| 0 | 0 | 0 |
| 0 | 1 | 90 |
| 1 | 0 | 270 |
| 1 | 1 | 180 |

The 10 MSBs of the HSP45102 drive the 10-bit HI5721 DAC which converts the NCO output into an analog waveform. The output filter connected to the DAC can be tailored to remove unwanted spurs for the desired carrier frequency. The controller is used to load the desired center frequency and control the HSP45102. The HI5721 coupled with the HSP45102 make an inexpensive PSK modulator with Spurious Free operation down to -76 dBc .


FIGURE 25. PSK MODULATOR USING THE HI5721 AND THE HSP45106 12-BIT NCO


FIGURE 26. PSK MODULATOR USING THE HI5721 AND THE HSP45102 12-BIT NCO

## Definition of Specifications

Integral Linearity Error, INL, is the measure of the worst case point that deviates from a best fit straight line of data values along the transfer curve.

Differential Linearity Error, DNL, is the measure of the step size output deviation from code to code. Ideally the step size should be 1 LSB. A DNL specification of 1 LSB or less guarantees monotonicity.
Feedthru is the measure of the undesirable switching noise coupled to the output.

Output Voltage Full Scale Settling Time, is the time required from the $50 \%$ point on the clock input for a full scale step to settle within an $1 / 2$ LSB error band.

Output Voltage Small Scale Settling Time, is the time required from the $50 \%$ point on the clock input for a 100 mV step to settle within an $1 / 2$ LSB error band. This is used by applications reconstructing highly correlated signals such as sine waves with more than 5 points per cycle.
Glitch Area, GE, is the switching transient appearing on the output during a code transition. It is measured as the area under the curve and expressed as a Volt-Time specification.

Differential Gain, $\Delta \mathbf{A}_{\mathbf{V}}$, is the gain error from an ideal sine wave with a normalized amplitude.
Differential Phase, $\Delta \Phi$, is the phase error from and ideal sine wave.

Signal to Noise Ratio, SNR, is the ratio of a fundamental to the noise floor of the analog output. The first 5 harmonics are ignored, and an output filter of $1 / 2$ the clock frequency is used to eliminate alias products.

Total Harmonic Distortion, THD, is the ratio of the DAC output fundamental to the RMS sum of the harmonics. The first 5 harmonics are included, and an output filter of $1 / 2$ the clock frequency is used to eliminate alias products.

Spurious Free Dynamic Range, SFDR, is the amplitude difference from a fundamental to the largest harmonically or non-harmonically related spur. A sine wave is loaded into the D/A and the output filtered at $1 / 2$ the clock frequency to eliminate noise from clocking alias terms.

Intermodulation Distortion, IMD is the measure of the sum and difference products produced when a two tone input is driven into the D/A. The distortion products created will arise at sum and difference frequencies of the two tones. IMD is

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## Dual-In-Line Plastic Packages (PDIP)



E28.6 (JEDEC MS-001-BF ISSUE D) 28 LEAD NARROW BODY DUAL-IN-LINE PLASTIC PACKAGE

| SYMBOL | INCHES |  | MILLIMETERS |  | NOTES |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | MIN | MAX | MIN | MAX |  |
| A | - | 0.250 | - | 6.35 | 4 |
| A1 | 0.015 | - | 0.39 | - | 4 |
| A2 | 0.125 | 0.195 | 3.18 | 4.95 | - |
| B | 0.014 | 0.022 | 0.356 | 0.558 | - |
| B1 | 0.030 | 0.070 | 0.77 | 1.77 | 8 |
| C | 0.008 | 0.015 | 0.204 | 0.381 | - |
| D | 1.380 | 1.565 | 35.1 | 39.7 | 5 |
| D1 | 0.005 | - | 0.13 | - | 5 |
| E | 0.600 | 0.625 | 15.24 | 15.87 | 6 |
| E1 | 0.485 | 0.580 | 12.32 | 14.73 | 5 |
| e | 0.10 | BSC | 2.5 | BSC | - |
| $\mathrm{e}_{\mathrm{A}}$ | 0.60 | BSC | 15.2 | BSC | 6 |
| $\mathrm{e}_{\mathrm{B}}$ | - | 0.700 | - | 17.78 | 7 |
| L | 0.115 | 0.200 | 2.93 | 5.08 | 4 |
| N | 28 |  | 28 |  | 9 |

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## Small Outline Plastic Packages (SOIC)



NOTES:

1. Symbols are defined in the "MO Series Symbol List" in Section 2.2 of Publication Number 95.
2. Dimensioning and tolerancing per ANSI Y14.5M-1982.
3. Dimension "D" does not include mold flash, protrusions or gate burrs. Mold flash, protrusion and gate burrs shall not exceed 0.15 mm ( 0.006 inch) per side.
4. Dimension "E" does not include interlead flash or protrusions. Interlead flash and protrusions shall not exceed 0.25 mm ( 0.010 inch) per side.
5. The chamfer on the body is optional. If it is not present, a visual index feature must be located within the crosshatched area.
6. " $L$ " is the length of terminal for soldering to a substrate.
7. " N " is the number of terminal positions.
8. Terminal numbers are shown for reference only.
9. The lead width " $B$ ", as measured 0.36 mm ( 0.014 inch) or greater above the seating plane, shall not exceed a maximum value of 0.61 mm ( 0.024 inch )
10. Controlling dimension: MILLIMETER. Converted inch dimensions are not necessarily exact.

[^0]:    IMD $=\frac{20 \log \text { (RMS of sum and difference distortion products) }}{\text { (RMS amplitude of the fundamental) }}$

